## Original Article

# Explicit analytical solutions for the average run length of modified EWMA control chart for ARX (p,r) processes 

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#### Abstract

Statistical process control (SPC) plays a necessary role in manufacturing industry processes. An essential tool for SPC used for monitoring, measuring, controlling, and improving quality in various fields is the control chart. The modified exponentially weighted moving average (modified EWMA) control chart is widely used in various fields, and a measure commonly used to elucidate its efficiency is average run length (ARL). The main purpose of this study is to derive explicit formulas for the $A R L$ to detect changes in the process mean of modified EWMA control chart for an autoregressive processes with explanatory variables (ARX(p,r)) with exponential white noise. In addition, the performances of the modified EWMA are compared with EWMA control charts based on the relative mean index (RMI). It was found that the explicit formulas for the $A R L$ of the modified EWMA control chart performed better than on the EWMA control chart for monitoring process mean.


Keywords: average run length, modified EWMA control chart, ARX process, explanatory variables, Integral equation

## 1. Introduction

Statistical process control (SPC) plays a necessary role in manufacturing industry processes and is used for monitoring, measuring, controlling and improving quality in various fields (science, economics, engineering, finance, medicine, etc.). An important SPC tool is the control chart which is used for detecting changes in process means. The first control chart, introduced by Shewhart (1931), was used for detecting large shifts in process means ( $>1.5 \sigma$ ) (Montgomery, 2012). The cumulative sum (CUSUM) control chart proposed by Page (1954) is a good alternative to the Shewhart control chart for detecting small shifts in process means ( $<1.5 \sigma$ ) (Montgomery, 2012), as has been indicated by comparative studies on the two (Hawkins \& Olwell, 1998; Lucas \& Saccucci, 1990). In addition, another option for detecting small shifts is the exponentially weighted moving

[^0]average (EWMA) control chart first presented by Roberts (1959), which has been used in various industries, However, these charts cannot be used directly for chemical and pharmaceutical processes due to the observations being frequently autocorrelated (Patel \& Divecha, 2011). The EWMA technique is used in SPC to monitor the results of manufacturing processes by tracking the moving average of the efficiency throughout the lifetime of the process.

The modified EWMA control chart developed by Patel and Divecha (2011) is a simplified EWMA control chart for detecting shifts in the process mean regardless of size. It is used in various fields, especially in the chemical industry, in which the processes are frequently autocorrelated. Past observations are considered (similar to the EWMA scheme) along with past changes as well as the latest change in the process mean. Khan, Aslam and Jun (2016) developed a new EWMA control chart based upon a modified EWMA statistic that considers the past and current behavior of the process; they compared it with the existing one by Patel and Divecha (2011) and found that the proposed control chart had the ability to detect shifts more quickly.

A commonly used measure for the efficiency of control charts is the average run length (ARL). Ryu, Wan and Kim (2010) applied in-control $A R L$ ( $A R L_{0}$ ), which refers to the average number of observations on the in-control process before a false out-of-control alarm is raised, as a measure of the false-alarm rate. The out-of-control $A R L\left(A R L_{1}\right)$, is the average number of observations required to detect a specific process mean shift and represents the ability to detect shifts in the process mean.

Various methods that can be used to find the $A R L$ of control charts have been proposed, such as Monte Carlo simulation, Markov chains, Martingales, numerical integration equations (NIEs), and explicit formulas. A NIE is a method for evaluating the $A R L$ that has many rules, namely the midpoint rule, trapezoidal rule, Simson's rule, and the Gauss-Legendre rule. In this study, we used the Gauss-Legendre rule. An explicit formula is a method for evaluating the $A R L$ that requires an integral equation for its derivation. In this study, we used the Fredholm integral equation of the second type (Mititelu, Areepong, Sukparungsee, \& Novikov, 2010). In 1959, Robert (1959) proposed an EWMA control chart by using Monte Carlo simulations to estimate the ARL. Crowder (1987) used an NIE approach to find the $A R L$ for a Gaussian distribution. Harris and Ross (1991) studied CUSUM with serially correlated observations via Monte Carlo simulations. Mititelu et al., (2010) used a linear Fredholm-type integral equation approach to derive explicit formulas for the $A R L$ in certain special cases. The $A R L$ for a CUSUM control chart has been found when the random observations follow a hyperexponential distribution and the ARL for an EWMA control chart with observations following a Laplace distribution. Suriyakat, Areepong, Sukparungsee and Mititelu (2012) derived explicit formulas for the ARL of the EWMA statistic for first-order autoregressive $(\operatorname{AR}(1))$ observations with errors following an exponential white noise process. Paichit (2016) used an NIE to find the exact expression for the $A R L$ of an EWMA control chart for an AR process with exogenous input (ARX(p)). Paichit (2017) presented an exact expression for the ARL of the control chart for an $\operatorname{ARX}(\mathrm{p})$ procedure. Explicit formulas for the ARL of a modified EWMA control chart for an exponential $\operatorname{AR}(1)$ process were presented by Phanthuna, Areepong and Sukparungsee (2018).

The main purpose of this study is to derive explicit formulas for the $A R L$ for detecting changes in the process mean of modified EWMA control chart based on Khan et al. (2016) for an autoregressive processes with explanatory variables (ARX(p,r)) with exponential white noise. In the present study, Fredholm-type integral equations are used to derive explicit formulas of $A R L_{0}$ and $A R L_{1}$. This paper is organized as follows. An introduction to the properties of control charts and the model for an $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process with exponential white noise is given in Section 2. The solutions for the ARLs of the EWMA and modified EWMA control charts for an $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process with exponential white noise are presented in Section 3. Next, the NIEs for the ARLs of the modified EWMA control charts are introduced in Section 4. Furthermore, numerical results for a comparison of the ARLs on the modified EWMA control charts for $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process with exponential white noise are offered in Section 5 and Section 6. The proposed explicit formulas are applied in Section 7. Finally, conclusions are given in Section 8.

## 2. The Properties of the Control Charts and ARX(p,r) Process with Exponential White Noise

### 2.1 The EWMA control chart

Roberts (1959) introduced the EWMA control chart for detecting small shifts in the process mean that is defined as
$Z_{t}=(1-\lambda) Z_{t-1}+\lambda Y_{t} \quad ; t=1,2,3, \ldots$,
where $Z_{t}$ is the EWMA statistic, $Y_{t}$ is the sequence of the $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process with exponential white noise and $\lambda$ is an exponential smoothing parameter $(0<\lambda \leq 1)$.

The stopping time will occur when an out-ofcontrol observation is firstly detected, which is sufficient to decide that the process is out-of-control. The stopping time $\tau_{b}$ for the EWMA control chart can be written as
$\tau_{b}=\inf \left\{t>0 ; Z_{t}>b\right\}$,
where $b$ is a constant parameter known as the upper control limit $(b>0)$. The upper side of the ARL for the $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process on the EWMA control chart with an initial value ( $Z_{0}=u$ ) can be found. Now, the function $L(u)$ is defined as
$L(u)=A R L=E_{\infty}\left(\tau_{b}\right) \geq T, Z_{0}=u$.
The mean and the variance of the EWMA control chart can be written as
$E\left(Z_{t}\right)=\mu$,
$\operatorname{Var}\left(Z_{t}\right)=\left(\frac{\lambda}{2-\lambda}\right) \sigma^{2}$,
and the upper control limit (UCL) and the lower control limit (LCL) of the EWMA control chart is defined as follows:
$L C L=\mu_{0}-L \sigma \sqrt{\frac{\lambda}{(2-\lambda)}}$,
$C L=\mu_{0}$,
$U C L=\mu_{0}+L \sigma \sqrt{\frac{\lambda}{(2-\lambda)}}$,
where $\mu_{0}$ is the target mean, $\sigma$ is the process standard deviation and $L$ is an appropriate control width limit ( $L>0$ ).

### 2.2 The modified EWMA control chart

Khan et al. (2016) developed a new EWMA control chart based upon the modified EWMA statistic that
considers the past and current behavior of the process. They compared the proposed chart with the existing modified EWMA control chart developed by Patel and Divecha (2011) that is a simplified EWMA control chart for detecting shifts of all sizes in the process mean under the assumption that the observations follow a normal distribution. The modified EWMA control chart proposed by Khan et al. (2016) is defined as
$M_{t}=(1-\lambda) M_{t-1}+\lambda Y_{t}+k\left(Y_{t}-Y_{t-1}\right) \quad ; t=1,2,3, \ldots$,
where $M_{t}$ is the modified EWMA statistic, $Y_{t}$ is the sequence of the $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process with exponential white noise, $\lambda$ is an exponential smoothing parameter $(0<\lambda \leq 1)$, and $k$ is a constant $(k>0)$.

The modified EWMA control chart is based on two constants, $\lambda$ and $k$, and comprises an extension to the existing EWMA control chart. The modified EWMA control chart by Khan et al. (2016) is reduced to the original EWMA control chart by Roberts (1959) if $k=0$ and is reduced to the control chart based on the modified EWMA control chart by Patel and Divecha (2011) if $k=1$.

The stopping time $\tau_{h}$ for the modified EWMA control chart can be written as
$\tau_{h}=\inf \left\{t>0 ; M_{t}>h\right\}$,
where $h$ is a constant parameter known as the upper control limit $(h>0)$. The upper side of the ARL for the ARX(p,r) process on the modified EWMA control chart with an initial value $\left(M_{0}=u\right)$ can be found. Now, we define the function $G(u)$ as
$A R L=G(u)=E_{\infty}\left(\tau_{h}\right) \geq T, M_{0}=u$,
where $T$ is a fixed number (should be large) and $E_{\infty}($.$) is the expectation under the assumption that observations \varepsilon_{t}$ have the distribution $F\left(y_{t}, \alpha\right)$.

The value of the mean and the variance of the modified EWMA control chart is defined as
$E\left(M_{t}\right)=\mu$,
$\operatorname{Var}\left(M_{t}\right)=\frac{\left(\lambda+2 \lambda k+2 k^{2}\right) \sigma^{2}}{(2-\lambda)}$,
and the $U C L$ and the $L C L$ of the modified EWMA control chart can be written as
$L C L=\mu_{0}-L \sigma \sqrt{\frac{\left(\lambda+2 \lambda k+2 k^{2}\right)}{(2-\lambda)}}$,
$C L=\mu_{0}$,
$U C L=\mu_{0}+L \sigma \sqrt{\frac{\left(\lambda+2 \lambda k+2 k^{2}\right)}{(2-\lambda)}}$,
where $\mu_{0}$ is the target mean, $\sigma^{2}$ is the process variance and $L$ is an appropriate control width limit $(L>0)$.

### 2.3 The ARX(p,r) process with exponential white noise

The ARX ( $\mathrm{p}, \mathrm{r}$ ) process is defined as
$Y_{t}=\delta+\phi_{1} Y_{t-1}+\phi_{2} Y_{t-2}+\ldots+\phi_{p} Y_{t-p}+\sum_{j=1}^{r} \beta_{j} X_{j}+\varepsilon_{t} \quad ; t=1,2,3, \ldots$,
where $\delta$ is a constant $(\delta \geq 0), \phi_{i}$ is an autoregressive coefficient for $i=1,2, \ldots, p\left(-1<\phi_{i}<1\right) ; \varepsilon_{t}$ is an independent and identically distributed (iid) sequence; $\varepsilon_{t} \square \operatorname{Exp}(\alpha) ; X_{j}$ are explanatory variables of $Y_{t}$; and $\beta_{j}$ are coefficients of
$X_{j} ; j=1,2, \ldots, r$. The initial value for the $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process mean is $Y_{t-1}, Y_{t-2}, \ldots, Y_{t-p}=1$ and the initial value for the explanatory variables $X_{1}, X_{2}, \ldots, X_{r}=1$.

## 3. Explicit Formulas for the ARLs of the Modified EWMA Control Chart for an ARX(p,r) Process with Exponential White Noise

Explicit formulas for the $A R L$ of the modified EWMA control chart for an ARX(p,r) process are derived as follows:

Substituting $Y_{t}$ from Equation (2.13) into Equation (2.7), then

$$
\begin{aligned}
M_{t} & =(1-\lambda) M_{t-1}+(\lambda+k) \delta+(\lambda+k) \phi_{1} Y_{t-1}+\ldots+(\lambda+k) \phi_{p} Y_{t-p} \\
& +(\lambda+k) \sum_{j=1}^{r} \beta_{j} X_{j}+(\lambda+k) \varepsilon_{t}-k Y_{t-1} .
\end{aligned}
$$

If $Y_{1}$ gives the out-of-control state for $M_{1}, M_{0}=u$ and $Y_{0}=v$, then
$M_{1}=(1-\lambda) u+(\lambda+k) \delta+(\lambda+k) \phi_{1} v+\ldots+(\lambda+k) \phi_{p} v+(\lambda+k) \sum_{j=1}^{r} \beta_{j} X_{j}+(\lambda+k) \varepsilon_{1}-k v$

If $\varepsilon_{1}$ is the in-control limit for $M_{1}$, then $0 \leq M_{1} \leq h$.
The function $G(u)$ can be derived by the Fredholm integral equation of the second type (Mititelu et al., 2010), and thus $G(u)$ can be written as

$$
\begin{equation*}
G(u)=1+\int G\left(M_{1}\right) f\left(\varepsilon_{1}\right) d\left(\varepsilon_{1}\right), \tag{3.1}
\end{equation*}
$$

by substituting $\varepsilon_{1}$ with $y$. Therefore, the function $G(u)$ is obtained as
$G(u)=1+\int_{0}^{h} L\left\{\begin{array}{l}(1-\lambda) u+(\lambda+k) \delta+(\lambda+k) \phi_{1} v+\ldots+(\lambda+k) \phi_{p} v \\ +(\lambda+k) \sum_{j=1}^{r} \beta_{j} X_{j}-k v+(\lambda+k) y\end{array}\right\} f(y) d y$.

Let $w=(1-\lambda) u+(\lambda+k) \delta+(\lambda+k) \phi_{1} v+\ldots+(\lambda+k) \phi_{p} v+(\lambda+k) \sum_{j=1}^{r} \beta_{j} X_{j}-k v+(\lambda+k) y$.

By changing the integral variable, we obtain the integral equation as follows:
$G(u)=1+\frac{1}{\lambda+k} \int_{0}^{h} G(w) f\left\{\frac{w-(1-\lambda) u}{(\lambda+k)}+\frac{k v}{(\lambda+k)}-\delta-v \sum_{i=1}^{p} \phi_{i}-\sum_{j=1}^{r} \beta_{j} X_{j}\right\} d w$.
If $Y_{t} \square \operatorname{Exp}(\alpha)$ the $f(y)=\frac{1}{\alpha} e^{\frac{-y}{\alpha}} ; y \geq 0$, so
$G(u)=1+\frac{1}{\lambda+k} \int_{0}^{h} G(w) \frac{1}{\alpha} e^{-\frac{1}{\alpha}\left\{\frac{w-(1-\lambda) u}{(\lambda+k)}+\frac{k v}{(\lambda+k)}-\delta-v \sum_{i=1}^{p} \phi_{i}-\sum_{j=1}^{r} \beta_{j} X_{j}\right\}} d w$.
Let the function $D(u)=e^{\frac{(1-\lambda) u}{\alpha(\lambda+k)}-\frac{k v}{\alpha(\lambda+k)}+\frac{\delta}{\alpha}+\frac{v \sum_{i=1}^{p} \phi_{i}}{\alpha}+\frac{\sum_{j=1}^{r} \beta_{j} X_{j}}{\alpha}}$, then we have
$G(u)=1+\frac{D(u)}{\alpha(\lambda+k)} \int_{0}^{h} L(w) e^{\frac{-w}{\alpha(\lambda+k)}} d w \quad ; 0 \leq u \leq h$.
Let $g=\int_{0}^{h} G(w) e^{\frac{-w}{\alpha(\lambda+k)}} d w$, then $G(u)=1+\frac{D(u)}{\alpha(\lambda+k)} \cdot g$. Consequently, we obtain
$G(u)=1+\frac{1}{\alpha(\lambda+k)} e^{\frac{(1-\lambda) u}{\alpha(\lambda+k)}-\frac{k v}{\alpha(\lambda+k)}+\frac{\delta}{\alpha}+\frac{v \sum_{i=1}^{p} \phi_{i}}{\alpha}+\frac{\sum_{j=1}^{r} \beta_{j} X_{j}}{\alpha}} \cdot g$.
Solving a constant $g$

$$
\begin{align*}
g & =\int_{0}^{h} G(w) e^{\frac{-w}{\alpha(\lambda+k)}} d w=\int_{0}^{h}\left[1+\frac{g}{\alpha(\lambda+k)} D(w)\right] e^{\frac{-w}{\alpha(\lambda+k)}} d w \\
& =\int_{0}^{h} e^{\frac{-w}{\alpha(\lambda+k)}} d w+\int_{0}^{h} \frac{g}{\alpha(\lambda+k)} D(w) \cdot e^{\frac{-w}{\alpha(\lambda+k)}} d w \\
& =-\alpha(\lambda+k)\left(e^{\frac{-h}{\alpha(\lambda+k)}}-1\right)+\frac{g e^{\frac{-k v}{\alpha(\lambda+k)}+\frac{\delta}{\alpha}+\frac{v \sum_{i=1}^{p} \phi_{i}}{\alpha}+\frac{\sum_{j=1}^{r} \beta_{j} X_{j}}{\alpha}}}{\alpha(\lambda+k)} \int_{0}^{h} e^{\frac{-\lambda w}{\alpha(\lambda+k)}} d w \\
& =-\alpha(\lambda+k)\left(e^{\frac{-h}{\alpha(\lambda+k)}}-1\right)-\frac{d e^{\frac{-k v}{\alpha(\lambda+k)}+\frac{\delta}{\alpha}+\frac{v \sum_{i=1}^{p} \phi_{i}}{\alpha}+\frac{\sum_{j=1}^{r} \beta_{j} X_{j}}{\alpha}}}{\lambda}\left(\frac{-\lambda h}{\lambda(\lambda+k)}-1\right) \\
g & =\frac{-\alpha(\lambda+k)\left(e^{\frac{-h}{\alpha(\lambda+k)}}-1\right)}{1+\frac{e^{\frac{-k v}{\alpha(\lambda+k)}+\frac{\delta}{\alpha}+\frac{v \sum_{i=1}^{p} \phi_{i}}{\alpha}+\frac{\sum_{j=1}^{r} \beta_{j} X_{j}}{\alpha}}}{\lambda}\left(\frac{-\lambda h}{\alpha(\lambda+k)}-1\right)} \tag{3.4}
\end{align*}
$$

Substituting $g$ from Equation (3.4) into Equation (3.3), then

$$
\begin{equation*}
G(u)=1-\frac{\lambda e^{\frac{(1-\lambda) u}{\alpha(\lambda+k)}}\left[e^{\frac{-h}{\alpha(\lambda+k)}}-1\right]}{\lambda e^{\frac{k v}{\alpha(\lambda+k)}-\frac{\delta}{\alpha}-\frac{v \sum_{i=1}^{p} \phi_{i}}{\alpha}-\frac{\sum_{j=1}^{r} \beta_{j} X_{j}}{\alpha}}+\left[e^{\frac{-\lambda h}{\alpha(\lambda+k)}}-1\right]} . \tag{3.5}
\end{equation*}
$$

When the process is in the in-control state with exponential parameter $\alpha=\alpha_{0}$, we obtain the explicit solution for $A R L_{0}$ as follows:


Similarly, when the process is in the out-of-control state with exponential parameter $\alpha=\alpha_{1}$, the explicit solution for $A R L_{1}$ can be written as

$$
\begin{equation*}
A R L_{1}=1-\frac{\lambda e^{\frac{(1-\lambda) u}{\alpha_{1}(\lambda+k)}}\left[e^{\frac{-h}{\alpha_{1}(\lambda+k)}}-1\right]}{\lambda e^{\frac{k v}{\alpha_{1}(\lambda+k)}-\frac{\delta}{\alpha_{1}}-\frac{v \sum_{i=1}^{p} \phi_{i}}{\alpha_{1}}-\frac{\sum_{j=1}^{r} \beta_{j} X_{j}}{\alpha_{1}}}+\left[e^{\frac{-\lambda h}{\alpha_{1}(\lambda+k)}}-1\right]} . \tag{3.7}
\end{equation*}
$$

## 4. The NIE for the ARL on the Modified EWMA Control Chart

An integral equation of the second type for the $A R L$ on the modified EWMA control chart for the ARX(p,r) process in Equation (3.5) can be approximated by using the quadrature formula. In this study, the Gauss-Legendre quadrature rule is applied as follows:

Given $f\left(a_{j}\right)=f\left\{\frac{a_{j}-(1-\lambda) a_{i}}{(\lambda+k)}+\frac{k v}{(\lambda+k)}-\delta-v \sum_{i=1}^{p} \phi_{i}-\sum_{j=1}^{r} \beta_{j} X_{j}\right\}$.
The approximation for the integral is in the form
$\int_{0}^{h} G(w) f(w) d w \approx \sum_{j=1}^{m} w_{j} f\left(a_{j}\right)$, where $a_{j}=\frac{h}{m}\left(j-\frac{1}{2}\right)$ and $w_{j}=\frac{h}{m} ; j=1,2, \ldots, m$.
Using the quadrature formula, the numerical approximation $\tilde{G}(u)$ for the integral equation can be found as a solution of the linear equations as follows:
$\tilde{G}\left(a_{i}\right)=1+\frac{1}{\lambda+k} \sum_{j=1}^{m} w_{j} \tilde{G}\left(a_{j}\right) f\left\{\frac{a_{j}-(1-\lambda) a_{i}}{(\lambda+k)}+\frac{k v}{(\lambda+k)}-\delta-v \sum_{i=1}^{p} \phi_{i}-\sum_{j=1}^{r} \beta_{j} X_{j}\right\} ; i=1,2, \ldots, m$.
Thus,
$\tilde{G}\left(a_{1}\right)=1+\frac{1}{\lambda+k} \sum_{j=1}^{m} w_{j} \tilde{G}\left(a_{j}\right) f\left\{\frac{a_{j}-(1-\lambda) a_{1}}{(\lambda+k)}+\frac{k v}{(\lambda+k)}-\delta-v \sum_{i=1}^{p} \phi_{i}-\sum_{j=1}^{r} \beta_{j} X_{j}\right\}$,
$\tilde{G}\left(a_{2}\right)=1+\frac{1}{\lambda+k} \sum_{j=1}^{m} w_{j} \tilde{G}\left(a_{j}\right) f\left\{\frac{a_{j}-(1-\lambda) a_{2}}{(\lambda+k)}+\frac{k v}{(\lambda+k)}-\delta-v \sum_{i=1}^{p} \phi_{i}-\sum_{j=1}^{r} \beta_{j} X_{j}\right\}$,
$\tilde{G}\left(a_{3}\right)=1+\frac{1}{\lambda+k} \sum_{j=1}^{m} w_{j} \tilde{G}\left(a_{j}\right) f\left\{\frac{a_{j}-(1-\lambda) a_{3}}{(\lambda+k)}+\frac{k v}{(\lambda+k)}-\delta-v \sum_{i=1}^{p} \phi_{i}-\sum_{j=1}^{r} \beta_{j} X_{j}\right\}$,
$\tilde{G}\left(a_{m}\right)=1+\frac{1}{\lambda+k} \sum_{j=1}^{m} w_{j} \tilde{G}\left(a_{j}\right) f\left\{\frac{a_{j}-(1-\lambda) a_{m}}{(\lambda+k)}+\frac{k v}{(\lambda+k)}-\delta-v \sum_{i=1}^{p} \phi_{i}-\sum_{j=1}^{r} \beta_{j} X_{j}\right\}$.
The set of $m$ equations with $m$ unknowns can be rewritten in matrix form. The column vector of $\tilde{G}\left(a_{i}\right)$ is $\mathbf{G}_{m \times 1}=\left(\tilde{G}\left(a_{1}\right), \tilde{G}\left(a_{2}\right), \ldots, \tilde{G}\left(a_{m}\right)\right)^{\prime}$. Since $\mathbf{1}_{m \times 1}=(1,1, \ldots, 1)^{\prime}$ is a column vector of ones and $\mathbf{R}_{m \times m}$ is a matrix, we can define $m$ to $m^{\text {th }}$ as elements of matrix $\mathbf{R}$ as follows:
$\left[R_{i j}\right] \approx \frac{1}{\lambda+k} w_{j} f\left\{\frac{a_{j}-(1-\lambda) a_{i}}{(\lambda+k)}+\frac{k v}{(\lambda+k)}-\delta-v \sum_{i=1}^{p} \phi_{i}-\sum_{j=1}^{r} \beta_{j} X_{j}\right\}$,
and $\mathbf{I}_{m}=\operatorname{diag}(1,1, \ldots, 1)$ is a unit matrix of order $m$. If $(\mathbf{I}-\mathbf{R})^{-1}$ exists, the numerical approximation for the integral equation in terms of the matrix can be written as
$\mathbf{G}_{m \times 1}=\left(\mathbf{I}_{m}-\mathbf{R}_{m \times m}\right)^{-1} \mathbf{1}_{m \times 1}$.
Finally, by substituting $a_{i}$ by $u$ in $\tilde{G}\left(a_{i}\right)$, the numerical integration equation for function $\tilde{G}(u)$ can be derived as
$\tilde{G}(u)=1+\frac{1}{\lambda+k} \sum_{j=1}^{m} w_{j} \tilde{G}\left(a_{j}\right) f\left\{\frac{a_{j}-(1-\lambda) u}{(\lambda+k)}+\frac{k v}{(\lambda+k)}-\delta-v \sum_{i=1}^{p} \phi_{i}-\sum_{j=1}^{r} \beta_{j} X_{j}\right\}$.

## 5. Comparison of the NIE Method and the Explicit Formulas

Here, a comparison of the efficacies of the NIE method ( $\tilde{G}(u)$ ) and the explicit formulas ( $G(u)$ ) for the ARL of an $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process on the modified EWMA control chart is presented. The parameter values were set as $A R L_{0}=370$ and 500 ; $\lambda=0.01,0.05,0.1$, and 0.2 ; the in-control parameter $\alpha_{0}=1$; and the shift size was varied as $0.01,0.02,0.03,0.04,0.05,0.1$, 0.3 , and 0.5 . In general, the popular setting of the initial value is equal to the expected value of the distribution. For setting the incontrol parameter, $\alpha_{0}=1$, which is the initial value as 1 . The coefficient has a value from -1 to 1 , which can be specified as any value. The configuration does not affect the accuracy of the explicit formulas and the NIE methods. The absolute percentage difference to measure the accuracy of the $A R L$ is defined as
$\operatorname{Diff}(\%)=\frac{|G(u)-\tilde{G}(u)|}{G(u)} \times 100$.
Equations (3.5) and (4.2) are used to evaluate the ARL on the modified EWMA control chart for an ARX(p,r) process with exponential white noise. The number of nodes equal to 500 iterations was used to obtain the $A R L$ results from the NIE method. The computations for the NIE method were carried out on a Windows 7 Professional 32-bit PC System with RAM of 2 GB and an AMD E1-1200 CPU.

The results in Tables 1-3 report the numerical values of the ARL derived from the explicit formulas and NIE method, and the absolute percentage difference between them. From the results, we can see that the $A R L$ values derived from the explicit formulas give the same results as the NIE method. The numerical approximations had an absolute percentage difference of less than $0.003 \%$. However, the computational time of the NIE method was $13.42-13.58 \mathrm{~s}$ whereas that of the explicit formulas was < 1 s .

Table 1. Comparison of the $A R L$ on a modified EWMA control chart using explicit formulas with the NIE method for ARX $(1,1)$ with $u=1$, $v=1, k=1, \beta_{1}=0.2$, and $A R L_{0}=370$

| $\lambda$ | $\delta$ | $\phi_{1}$ | $h$ | shift | Explicit | NIE | Time ${ }^{\text {a }}$ | Diff\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.05 | 0 | 0.1 | 2.11284 | 0.00 | 370.514622 | 370.514167 | 13.468 | 0.000123 |
|  |  |  |  | 0.01 | 185.632808 | 185.632635 | 13.555 | 0.000093 |
|  |  |  |  | 0.02 | 123.215119 | 123.215018 | 13.494 | 0.000082 |
|  |  |  |  | 0.03 | 91.885107 | 91.885037 | 13.428 | 0.000076 |
|  |  |  |  | 0.04 | 73.065410 | 73.065357 | 13.551 | 0.000072 |
|  |  |  |  | 0.05 | 60.520993 | 60.520951 | 13.552 | 0.000068 |
|  |  |  |  | 0.10 | 32.116753 | 32.116734 | 13.504 | 0.000058 |
|  |  |  |  | 0.30 | 10.731776 | 10.731772 | 13.546 | 0.000037 |
|  |  |  |  | 0.50 | 6.457709 | 6.457707 | 13.440 | 0.000026 |
|  |  | -0.1 | 2.61195 | 0.00 | 370.424900 | 370.424156 | 13.511 | 0.000201 |
|  |  |  |  | 0.01 | 274.686377 | 274.685905 | 13.563 | 0.000172 |
|  |  |  |  | 0.02 | 214.349128 | 214.348800 | 13.478 | 0.000153 |
|  |  |  |  | 0.03 | 173.294237 | 173.293995 | 13.511 | 0.000140 |
|  |  |  |  | 0.04 | 143.823485 | 143.823298 | 13.446 | 0.000130 |
|  |  |  |  | 0.05 | 121.811602 | 121.811453 | 13.445 | 0.000122 |
|  |  |  |  | 0.10 | 64.531777 | 64.531713 | 13.421 | 0.000098 |
|  |  |  |  | 0.30 | 17.824627 | 17.824616 | 13.541 | 0.000060 |
|  |  |  |  | 0.50 | 9.519466 | 9.519462 | 13.452 | 0.000042 |
| 0.10 | 1 | 0.2 | 0.69141 | 0.00 | 370.555941 | 370.555865 | 13.502 | 0.000021 |
|  |  |  |  | 0.01 | 90.098635 | 90.098626 | 13.498 | 0.000010 |
|  |  |  |  | 0.02 | 51.385975 | 51.385971 | 13.460 | 0.000008 |
|  |  |  |  | 0.03 | 35.997312 | 35.997309 | 13.434 | 0.000007 |
|  |  |  |  | 0.04 | 27.736604 | 27.736602 | 13.467 | 0.000007 |
|  |  |  |  | 0.05 | 22.584474 | 22.584472 | 13.485 | 0.000006 |
|  |  |  |  | 0.10 | 11.823565 | 11.823565 | 13.518 | 0.000005 |
|  |  |  |  | 0.30 | 4.369675 | 4.369675 | 13.506 | 0.000003 |
|  |  |  |  | 0.50 | 2.902154 | 2.902154 | 13.467 | 0.000002 |
|  |  | -0.2 | 1.04870 | 0.00 | 370.273926 | 370.273736 | 13.537 | 0.000052 |
|  |  |  |  | 0.01 | 105.208634 | 105.208608 | 13.519 | 0.000025 |
|  |  |  |  | 0.02 | 61.437849 | 61.437836 | 13.532 | 0.000020 |
|  |  |  |  | 0.03 | 43.452288 | 43.452281 | 13.542 | 0.000018 |
|  |  |  |  | 0.04 | 33.653645 | 33.653639 | 13.449 | 0.000017 |
|  |  |  |  | 0.05 | 27.489870 | 27.489866 | 13.471 | 0.000016 |
|  |  |  |  | 0.10 | 14.478770 | 14.478768 | 13.508 | 0.000013 |
|  |  |  |  | 0.30 | 5.327500 | 5.327500 | 13.488 | 0.000008 |
|  |  |  |  | 0.50 | 3.494115 | 3.494115 | 13.434 | 0.000005 |

${ }^{\text {a }}$ The computational times for the NIE methods in seconds (PC System: Windows 7 Professional 32-bit, RAM: 2 GB and CPU: AMD E1-1200)
Table 2. Comparison of the $A R L$ on a modified EWMA control chart using explicit formulas with the NIE method for ARX $(2,1)$ with $u=1, v=1, \delta=0, k=1, \beta_{1}=0.2$, and $A R L_{0}=370$.

| $\lambda$ | $\phi_{1}$ | $\phi_{2}$ | $h$ | shift | Explicit | NIE | Time | Diff\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.05 | 0.1 | 0.1 | 1.90196 | 0.00 | 370.104536 | 370.104178 | 13.492 | 0.000097 |
|  |  |  |  | 0.01 | 164.156587 | 164.156470 | 13.512 | 0.000072 |
|  |  |  |  | 0.02 | 105.192627 | 105.192560 | 13.467 | 0.000063 |
|  |  |  |  | 0.03 | 77.258066 | 77.258020 | 13.551 | 0.000059 |
|  |  |  |  | 0.04 | 60.970239 | 60.970204 | 13.466 | 0.000056 |
|  |  |  |  | 0.05 | 50.307351 | 50.307324 | 13.532 | 0.000054 |
|  |  |  |  | 0.10 | 26.685128 | 26.685116 | 13.545 | 0.000046 |
|  |  |  |  | 0.30 | 9.216663 | 9.216660 | 13.436 | 0.000029 |
|  |  |  |  | 0.50 | 5.688211 | 5.688210 | 13.529 | 0.000020 |
|  |  | -0.1 | 2.34842 | 0.00 | 370.111274 | 370.110694 | 13.520 | 0.000157 |
|  |  |  |  | 0.01 | 218.233870 | 218.233600 | 13.487 | 0.000124 |
|  |  |  |  | 0.02 | 153.301535 | 153.301368 | 13.495 | 0.000109 |
|  |  |  |  | 0.03 | 117.350069 | 117.349952 | 13.416 | 0.000100 |
|  |  |  |  | 0.04 | 94.565641 | 94.565553 | 13.479 | 0.000094 |
|  |  |  |  | 0.05 | 78.865508 | 78.865438 | 13.492 | 0.000089 |
|  |  |  |  | 0.10 | 41.847694 | 41.847663 | 13.492 | 0.000074 |
|  |  |  |  | 0.30 | 13.172037 | 13.172030 | 13.492 | 0.000047 |
|  |  |  |  | 0.50 | 7.603031 | 7.603028 | 13.517 | 0.000033 |

Table 2. Continued.

| $\lambda$ | $\phi_{1}$ | $\phi_{2}$ | $h$ | shift | Explicit | NIE | Time | Diff\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.10 | 0.1 | 0.2 | 1.78838 | 0.00 | 370.299172 | 370.298515 | 13.519 | 0.000178 |
|  |  |  |  | 0.01 | 144.464904 | 144.464768 | 13.518 | 0.000094 |
|  |  |  |  | 0.02 | 89.685034 | 89.684969 | 13.459 | 0.000073 |
|  |  |  |  | 0.03 | 65.007924 | 65.007883 | 13.455 | 0.000063 |
|  |  |  |  | 0.04 | 50.973254 | 50.973225 | 13.535 | 0.000057 |
|  |  |  |  | 0.05 | 41.920612 | 41.920590 | 13.490 | 0.000052 |
|  |  |  |  | 0.10 | 22.222112 | 22.222103 | 13.425 | 0.000041 |
|  |  |  |  | 0.30 | 7.893825 | 7.893823 | 13.482 | 0.000024 |
|  |  |  |  | 0.50 | 4.987173 | 4.987172 | 13.499 | 0.000016 |
|  |  | -0.2 | 2.78993 | 0.00 | 370.115966 | 370.114002 | 13.501 | 0.000531 |
|  |  |  |  | 0.01 | 286.090889 | 286.089671 | 13.542 | 0.000426 |
|  |  |  |  | 0.02 | 228.394081 | 228.393273 | 13.492 | 0.000354 |
|  |  |  |  | 0.03 | 187.010941 | 187.010376 | 13.531 | 0.000302 |
|  |  |  |  | 0.04 | 156.285272 | 156.284860 | 13.569 | 0.000264 |
|  |  |  |  | 0.05 | 132.822686 | 132.822375 | 13.438 | 0.000234 |
|  |  |  |  | 0.10 | 70.157635 | 70.157527 | 13.440 | 0.000153 |
|  |  |  |  | 0.30 | 18.713286 | 18.713273 | 13.557 | 0.000072 |
|  |  |  |  | 0.50 | 9.832924 | 9.832919 | 13.520 | 0.000047 |
| 0.20 | 0.2 | 0.1 | 1.95666 | 0.00 | 370.295141 | 370.292831 | 13.437 | 0.000624 |
|  |  |  |  | 0.01 | 137.992552 | 137.992202 | 13.490 | 0.000253 |
|  |  |  |  | 0.02 | 84.820251 | 84.820109 | 13.462 | 0.000168 |
|  |  |  |  | 0.03 | 61.246548 | 61.246469 | 13.427 | 0.000130 |
|  |  |  |  | 0.04 | 47.941844 | 47.941792 | 13.486 | 0.000108 |
|  |  |  |  | 0.05 | 39.398626 | 39.398589 | 13.534 | 0.000093 |
|  |  |  |  | 0.10 | 20.908407 | 20.908394 | 13.466 | 0.000060 |
|  |  |  |  | 0.30 | 7.523560 | 7.523557 | 13.512 | 0.000028 |
|  |  |  |  | 0.50 | 4.802271 | 4.802270 | 13.539 | 0.000018 |
|  |  | -0.1 | 2.49307 | 0.00 | 370.002909 | 369.998734 | 13.478 | 0.001128 |
|  |  |  |  | 0.01 | 183.558057 | 183.556989 | 13.456 | 0.000582 |
|  |  |  |  | 0.02 | 121.435201 | 121.434716 | 13.457 | 0.000399 |
|  |  |  |  | 0.03 | 90.409051 | 90.408773 | 13.539 | 0.000307 |
|  |  |  |  | 0.04 | 71.822583 | 71.822402 | 13.520 | 0.000252 |
|  |  |  |  | 0.05 | 59.455236 | 59.455108 | 13.515 | 0.000215 |
|  |  |  |  | 0.10 | 31.519801 | 31.519760 | 13.498 | 0.000129 |
|  |  |  |  | 0.30 | 10.562568 | 10.562562 | 13.519 | 0.000054 |
|  |  |  |  | 0.50 | 6.382784 | 6.382781 | 13.433 | 0.000033 |

Table 3. Comparison of the $A R L$ on a modified EWMA control chart using explicit formulas with the NIE method for ARX $(2,1)$ with $u=1, v=1, \delta=0, k=1, \phi_{1}=0.1, \phi_{2}=-0.2, \beta_{1}=0.2$, and $A R L_{0}=500$.

| shift | $\lambda=0.01, h=2.48512$ |  |  |  | $\lambda=0.05, h=2.61385$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Explicit | NIE | Time | Diff\% | Explicit | NIE | Time | Diff\% |
| 0.00 | 500.488509 | 500.487979 | 13.458 | 0.000106 | 500.640854 | 500.639672 | 13.476 | 0.000236 |
| 0.01 | 331.637724 | 331.637386 | 13.484 | 0.000102 | 340.395524 | 340.394878 | 13.463 | 0.000190 |
| 0.02 | 243.153820 | 243.153579 | 13.448 | 0.000099 | 252.391615 | 252.391203 | 13.531 | 0.000163 |
| 0.03 | 189.153991 | 189.153809 | 13.490 | 0.000096 | 197.352918 | 197.352629 | 13.536 | 0.000146 |
| 0.04 | 153.035120 | 153.034976 | 13.469 | 0.000094 | 160.016146 | 160.015932 | 13.469 | 0.000134 |
| 0.05 | 127.342375 | 127.342258 | 13.468 | 0.000092 | 133.230089 | 133.229922 | 13.533 | 0.000125 |
| 0.10 | 64.915512 | 64.915458 | 13.506 | 0.000083 | 67.592092 | 67.592025 | 13.497 | 0.000099 |
| 0.30 | 17.675818 | 17.675808 | 13.491 | 0.000056 | 18.040792 | 18.040781 | 13.502 | 0.000060 |
| 0.50 | 9.459167 | 9.459163 | 13.546 | 0.000040 | 9.576707 | 9.576703 | 13.510 | 0.000042 |
| shift | $\lambda=0.1, h=2.79202$ |  |  |  | $\lambda=0.2, h=3.22379$ |  |  |  |
|  | Explicit | NIE | Time | Diff\% | Explicit | NIE | Time | Diff\% |
| 0.00 | 500.386457 | 500.383045 | 13.496 | 0.000682 | 500.609662 | 500.595309 | 13.455 | 0.002867 |
| 0.01 | 358.298531 | 358.296709 | 13.537 | 0.000508 | 434.146693 | 434.136038 | 13.552 | 0.002454 |
| 0.02 | 272.247864 | 272.246767 | 13.458 | 0.000403 | 368.724286 | 368.716686 | 13.482 | 0.002061 |

Table 3. Continued.

| shift | $\lambda=0.1, h=2.79202$ |  |  |  |  | $\lambda=0.2, h=3.22379$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Explicit | NIE | Time | Diff $\%$ | Explicit | NIE | Time | Diff $\%$ |
| 0.03 | 215.455768 | 215.455048 | 13.496 | 0.000334 | 310.585722 | 310.580379 | 13.495 | 0.001720 |
| 0.04 | 175.682830 | 175.682330 | 13.486 | 0.000285 | 261.603168 | 261.599405 | 13.447 | 0.001438 |
| 0.05 | 146.584892 | 146.584527 | 13.469 | 0.000249 | 221.388663 | 221.385984 | 13.530 | 0.001210 |
| 0.10 | 73.817022 | 73.816906 | 13.579 | 0.000157 | 108.236492 | 108.235857 | 13.506 | 0.000586 |
| 0.30 | 18.955138 | 18.955124 | 13.516 | 0.000072 | 23.381342 | 23.381309 | 13.507 | 0.000139 |
| 0.50 | 9.895165 | 9.895160 | 13.461 | 0.000047 | 11.381464 | 11.381456 | 13.513 | 0.000072 |

## 6. Comparison of the ARLs on the EWMA with modified EWMA control charts

After verifying the accuracy of the explicit formulas in the previous section, we used simulated data and the relative mean index (RMI) to compare the performances of the ARL of an ARX(p,r) process on EWMA and modified EWMA control charts. The RMI is defined as
$R M I=\frac{1}{n} \sum_{i=1}^{n}\left(\frac{A R L_{\text {shift }, i}-\operatorname{Min}\left[A R L_{\text {shift }, i}\right]}{\operatorname{Min}\left[A R L_{\text {shift }, i}\right]}\right)$.
where $A R L_{\text {shift }, i}$ is the $A R L$ of the control chart when the position process shift, shift, $i$ is the shift size for $i=1,2, \ldots, n$, $\operatorname{Min}\left[A R L_{\text {shift,i }}\right]$ denotes the smallest $A R L$ of two control charts in comparison when the position process shift. The control chart with the smallest RMI performs the best in detecting mean changes on the whole.

For the comparison of the ARLs on the EWMA and modified EWMA control charts for an ARX $(1,1)$ process, the parameter values were set as $A R L_{0}=370 ; \lambda=0.05,0.1$, and 0.2 ; the in-control parameter $\alpha_{0}=1$; the shift size was varied as $0.001,0.003,0.005,0.007,0.009,0.01,0.03,0.05,0.07$ and 0.09 . The results are reported in Table 4.

Table 4. Comparison of the $A R L$ of EWMA and modified EWMA control charts using explicit formulas for an ARX $(1,1)$ with $u=1, v=1, \delta=0, k=40 \lambda, \beta_{1}=0.2$, and $A R L_{0}=370$.

| shift | $\lambda=0.05, \phi_{1}=0.2$ |  | $\lambda=0.1, \phi_{1}=0.2$ |  | $\lambda=0.2, \phi_{1}=0.2$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EWMA $b=2.5496 \times 10^{-8}$ | Modified EWMA $h=1.3590441$ | $\begin{gathered} \text { EWMA } \\ b=0.00107964 \end{gathered}$ | Modified EWMA $h=2.7665764$ | $\begin{gathered} \text { EWMA } \\ b=0.04441 \end{gathered}$ | Modified EWMA $h=5.734902$ |
| 0.000 | 370.071291 | 370.0768919 | 370.004307 | 370.003373 | 370.722568 | 370.715572 |
| 0.001 | 362.264617 | 257.030787* | 365.787507 | 239.166659* | 362.075941 | 233.363671* |
| 0.003 | 347.186399 | 159.726241* | 357.521610 | 140.347811* | 345.767724 | 134.327916* |
| 0.005 | 332.792484 | 115.984299* | 349.473732 | 99.484050* | 330.655613 | 94.494822* |
| 0.007 | 319.049437 | 91.124031* | 341.637371 | 77.151829* | 316.615806 | 72.994088* |
| 0.009 | 305.925567 | 75.090081* | 334.006238 | 63.075235* | 303.540954 | 59.537517* |
| 0.010 | 299.586374 | 69.033841* | 330.265724 | 57.823254* | 297.335678 | 54.535706* |
| 0.030 | 198.799944 | 26.743266* | 264.852791 | 22.105174* | 206.492192 | 20.787108* |
| 0.050 | 134.056104 | 16.821242* | 214.163689 | 13.957965* | 153.166554 | 13.153305* |
| 0.070 | 91.808369 | 12.393346* | 174.541323 | 10.348427* | 118.601180 | 9.778282* |
| 0.090 | 63.828457 | 9.886695* | 143.313881 | 8.311410* | 94.690406 | 7.875239* |
| RMI | 3.763440 | 0 | 7.445925 | 0 | 5.824404 | 0 |
| shift | $\lambda=0.05, \phi_{1}=-0.2$ |  | $\lambda=0.1, \phi_{1}=-0.2$ |  | $\lambda=0.2, \phi_{1}=-0.2$ |  |
|  | $\begin{gathered} \text { EWMA } \\ b=3.8036 \times 10^{-8} \end{gathered}$ | Modified EWMA $h=2.0452044$ | $\begin{gathered} \text { EWMA } \\ b=0.0016149 \end{gathered}$ | Modified EWMA $h=4.200333$ | $\begin{gathered} \text { EWMA } \\ b=0.067334 \end{gathered}$ | Modified EWMA $h=8.88252$ |
| 0.000 | 370.075490 | 370.074437 | 370.035318 | 370.040056 | 370.017072 | 370.021854 |
| 0.001 | 362.413120 | 272.589846* | 365.971526 | 257.425111* | 362.407567 | 254.808465* |
| 0.003 | 347.604772 | 178.698291* | 358.000435 | 160.267524* | 347.947355 | 157.288491* |
| 0.005 | 333.457209 | 133.038467* | 350.232942 | 116.523643* | 334.419802 | 113.936839* |

Table 4. Continued.

| shift | $\lambda=0.05, \phi_{1}=-0.2$ |  | $\lambda=0.1, \phi_{1}=-0.2$ |  | $\lambda=0.2, \phi_{1}=-0.2$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EWMA | Modified EWMA | EWMA | Modified EWMA | EWMA | Modified EWMA |
|  | $b=3.8036 \times 10^{-8}$ | $h=2.0452044$ | $b=0.0016149$ | $h=4.200333$ | $b=0.067334$ | $h=8.88252$ |
| 0.007 | 319.938646 | 106.040681* | 342.663148 | 91.643263* | 321.740040 | 89.431083* |
| 0.009 | 307.018935 | 88.205073* | 335.285344 | 75.588906* | 309.833149 | 73.676321* |
| 0.010 | 300.774653 | 81.379575* | 331.666704 | 69.523408* | 304.148484 | 67.735772* |
| 0.030 | 201.120167 | 32.306069* | 268.119397 | 27.141638* | 218.327779 | 26.405507* |
| 0.050 | 136.616346 | 20.420367* | 218.476210 | 17.187944* | 165.516539 | 16.743211* |
| 0.070 | 94.217093 | 15.067503* | 179.369496 | 12.742094* | 130.215179 | 12.432517* |
| 0.090 | 65.938916 | 12.022993* | 148.318390 | 10.222777* | 105.253345 | 9.990907* |
| RMI | 3.062808 | 0 | 6.078151 | 0 | 4.802528 | 0 |

*The smallest $A R L$ on each shift size according to the case.
For the $A R L$ comparison for an $\operatorname{ARX}(2,1)$ process on the EWMA and modified EWMA control charts, the parameter values were set as $A R L_{0}=500 ; \lambda=0.05,0.1$, and 0.2 ; the in-control parameter $\alpha_{0}=1$; shift sizes of $0.001,0.003,0.005$, $0.007,0.009,0.01,0.03,0.05,0.07$ and 0.09 . The results are reported in Table 5.

Table 5. Comparison of the $A R L$ of EWMA and modified EWMA control charts using explicit formulas for an $\operatorname{ARX}(2,1)$ with $u=1, v=1$,
$\delta=2, k=50 \lambda, \beta_{1}=0.3$ and $A R L_{0}=500$.

| shift | $\lambda=0.05, \phi_{1}=0.1, \phi_{1}=-0.2$ |  | $\lambda=0.1, \phi_{1}=0.1, \phi_{1}=-0.1$ |  | $\lambda=0.2, \phi_{1}=0.1, \phi_{1}=0.1$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { EWMA } \\ b=1.5491 \times 10^{-8} \end{gathered}$ | Modified EWMA $h=0.7568155$ | $\begin{gathered} \text { EWMA } \\ b=0.00058356 \end{gathered}$ | Modified EWMA $h=1.378502$ | $\begin{gathered} \text { EWMA } \\ b=0.014952 \end{gathered}$ | Modified EWMA $h=2.277413$ |
| 0.000 | 500.060978 | 500.076069 | 500.324113 | 500.360304 | 500.029224 | 500.022472 |
| 0.001 | 489.114475 | 267.090908* | 494.127012 | 239.961773* | 480.592452 | 221.762202 |
| 0.003 | 467.997069 | 138.496237* | 481.998019 | 117.893325* | 445.500726 | 105.295630 |
| 0.005 | 447.870153 | 93.629467* | 470.213191 | 78.325628* | 414.691287 | 69.234304 |
| 0.007 | 428.683824 | 70.801160* | 458.761545 | 58.745762* | 387.433378 | 51.680381 |
| 0.009 | 410.390862 | 56.975292* | 447.632483 | 47.062407* | 363.153404 | 41.295851 |
| 0.010 | 401.565333 | 51.923525* | 442.185713 | 42.825869* | 351.983744 | 37.546730 |
| 0.030 | 262.306360 | 19.020934* | 347.882344 | 15.647366* | 210.659066 | 13.700820 |
| 0.050 | 174.194272 | 11.857221* | 276.201620 | 9.822354* | 143.484292 | 8.635854 |
| 0.070 | 117.530522 | 8.724851* | 221.192183 | 7.284761* | 104.938276 | 6.434339 |
| 0.090 | 80.526574 | 6.969808* | 178.593387 | 5.865033* | 80.339327 | 5.203939 |
| RMI | 7.449113 | 0 | 14.096343 | 0 | 9.179088 | 0 |
| shift | $\lambda=0.05, \phi_{1}=0.2, \phi_{1}=-0.1$ |  | $\lambda=0.1, \phi_{1}=0.2, \phi_{1}=0.1$ |  | $\lambda=0.2, \phi_{1}=0.2, \phi_{1}=0.2$ |  |
|  | EWMA | Modified EWMA | EWMA | Modified EWMA | EWMA | Modified EWMA |
|  | $b=1.2685 \times 10^{-8}$ | $h=0.6187533$ | $b=0.00043188$ | $h=1.0175587$ | $b=0.0122187$ | $h=1.85691$ |
| 0.000 | 500.141339 | 500.150484 | 500.174945 | 500.189478 | 500.055307 | 500.024614 |
| 0.001 | 489.095541 | 259.298533* | 493.822612 | 228.318970* | 479.729360 | 214.054265* |
| 0.003 | 467.792945 | 132.316088* | 481.395919 | 109.704783* | 443.211639 | 100.188030* |
| 0.005 | 447.497611 | 88.958619* | 469.329752 | 72.374872* | 411.339382 | 65.592229* |
| 0.007 | 428.158412 | 67.081769* | 457.612366 | 54.098310* | 383.287724 | 48.862371* |
| 0.009 | 409.726985 | 53.891761* | 446.232438 | 43.253693* | 358.416006 | 38.999212* |
| 0.010 | 400.837290 | 49.083498* | 440.665594 | 39.332505* | 347.010479 | 35.444488* |
| 0.030 | 260.830440 | 17.912907* | 344.589520 | 14.318623* | 204.669047 | 12.911676* |
| 0.050 | 172.580252 | 11.160506* | 272.008910 | 8.990081* | 138.296605 | 8.143100* |
| 0.070 | 116.034271 | 8.212396* | 216.634577 | 6.672959* | 100.601078 | 6.072667* |
| 0.090 | 79.236668 | 6.562091* | 173.992869 | 5.378034* | 76.705241 | 4.916320* |
| RMI | 7.883248 | 0 | 15.215424 | 0 | 9.476407 | 0 |

*The smallest $A R L$ on each shift size according to the case.

From the results in Tables 4 and 5, it is evident that the $A R L$ values derived from the explicit formulas for the modified EWMA control chart are less than those for the EWMA control chart for every value of $\lambda$. For example, in Table 4, when $\phi_{1}=0.2, \lambda=0.05$ and shift $=0.05$, the $A R L$ is 332.792484 from the EWMA control chart while the $A R L$ is 115.984299 from the modified EWMA control chart, which corresponds to the RMI values for the modified EWMA control chart being less than those for the EWMA control chart.

## 7. Application

In Section 6, we compared the performance of the ARL of an ARX(p,r) process on EWMA and modified EWMA control charts by using simulation data. The results show that the $A R L$ values derived from the explicit formulas for the modified EWMA control chart were shorter than those for the EWMA control chart in every case. Hence, we applied the explicit formulas for the $A R L$ s on the EWMA and modified EWMA control charts for an $\operatorname{ARX}(1,1)$ process using 55 real-world data observations on the value of exports and imports of agricultural products to and from Thailand (Unit: Ten billion baht) from January 2016 to July 2019, where the value of the imports is the explanatory variable (data from the Office of Agricultural Economics of Thailand (2019)) to confirm the above results. The parameters were set as $\lambda=0.05,0.1$, and $0.2 ; \alpha_{0}=u=0.589259$; shift size values of $0.001,0.003,0.005,0.007,0.009,0.01,0.03,0.05,0.07$, and 0.09 ; and autoregressive coefficients $\phi_{1}=0.326152, \delta=6.652233$, $v=10.4918, \beta_{1}=0.933313$, and $X_{1}=4.1439$. The results are given in Table 6.

Another ARL comparison for an $\operatorname{ARX}(2,1)$ process on the modified EWMA control charts was conducted using realworld data on the price of cassava (unit: Baht per kilogram, data from the Office of Agricultural Economics of Thailand (2019)) and diesel oil (unit: Baht per liter, data from Petroleum Authority of Thailand (2019)), with the latter being the explanatory variable. The parameters used were $\lambda=0.1,0.15$ and $0.2 ; \alpha_{0}=u=0.136281$; shift size values of $0.0001,0.0003,0.0005$, $0.0007,0.0009,0.001,0.003,0.005,0.007$, and 0.009 ; and autoregressive coefficients $\phi_{1}=0.623567$ and $\phi_{2}=0.292098$, $\delta=0, v=1.88, \beta_{1}=0.064905$, and $X_{1}=25.62$. The results are summarized in Table 7.

Table 6. Comparison of the $A R L$ of $\operatorname{ARX}(1,1)$ of EWMA and modified EWMA control charts for the value of exports and imports of agricultural products for $A R L_{0}=370$.

| shift | $\lambda=0.05(k=100 \lambda)^{\mathbf{a}}$ |  | $\lambda=0.1 \quad(k=40 \lambda)$ |  | $\lambda=0.2(k=60 \lambda)$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EWMA | Modified EWMA | EWMA | Modified EWMA | EWMA | Modified EWMA |
|  | $b=3.27104 \times 10^{-18}$ | $h=0.007128814$ | $b=1.3617 \times 10^{-13}$ | $h=0.0044711692$ | $b=5.446519 \times 10^{-12}$ | $h=0.0153495067$ |
| 0.000 | 374.505189 | 374.510271 | 370.015353 | 370.013368 | 370.026479 | 370.026204 |
| 0.001 | 348.463281 | 80.027591* | 348.920418 | 79.529679* | 276.359424 | 71.606027* |
| 0.003 | 301.920274 | 31.405097* | 310.520857 | 31.227647* | 178.925791 | 27.747820* |
| 0.005 | 261.864143 | 19.690008* | 276.644980 | 19.575453* | 128.916300 | 17.383968* |
| 0.007 | 227.356776 | 14.422145* | 246.734101 | 14.334171* | 98.643720 | 12.748838* |
| 0.009 | 197.600498 | 11.428518* | 220.280627 | 11.355250* | 78.453653 | 10.121645* |
| 0.010 | 184.287726 | 10.369330* | 208.221352 | 10.301213* | 70.713067 | 9.193284* |
| 0.030 | 48.289170 | 3.899445* | 70.946841 | 3.863411* | 17.089659 | 3.535219* |
| 0.050 | 14.280238 | 2.596183* | 26.449591 | 2.568076* | 6.766353 | 2.397466* |
| 0.070 | 5.028239 | 2.046506* | 10.869219 | 2.022750* | 3.406272 | 1.917426* |
| 0.090 | 2.310792 | 1.748461* | 5.049280 | 1.727746* | 2.092499 | 1.656939* |
| RMI | 8.975697 | 0 | 11.224773 | 0 | 4.159967 | 0 |


Table 7. Comparison of the $A R L$ of $\operatorname{ARX}(2,1)$ of EWMA and modified EWMA control charts for the price of cassava and diesel oil for $k=40 \lambda$ and $A R L_{0}=500$.

| shift | $\lambda=0.1$ |  | $\lambda=0.15$ |  | $\lambda=0.2$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EWMA | Modified EWMA | EWMA | Modified EWMA | EWMA | Modified EWMA |
|  | $b=1.2971 \times 10^{-14}$ | $b=6.399136 \times 10^{-6}$ | $b=2.1239 \times 10^{-13}$ | $b=9.600579 \times 10^{-6}$ | $b=4.0308 \times 10^{-13}$ | $b=1.2801949 \times 10^{-5}$ |
| 0.0000 | 500.039396 | 500.039009 | 500.179242 | 500.174921 | 500.226696 | 500.227872 |
| 0.0001 | 486.931023 | 108.038894* | 473.487004 | 101.389201* | 417.839400 | 98.180795* |
| 0.0003 | 461.702687 | 42.328712* | 426.334701 | 39.364297* | 311.758448 | 37.955938* |
| 0.0005 | 437.968562 | 26.452894* | 385.987063 | 24.571033* | 246.391305 | 23.680218* |

Table 7. Continued.

| shift | $\lambda=0.1$ |  | $\lambda=0.15$ |  | $\lambda=0.2$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { EWMA } \\ b=1.2971 \times 10^{-14} \end{gathered}$ | $\begin{gathered} \text { Modified EWMA } \\ b=6.399136 \times 10^{-6} \end{gathered}$ | $\begin{gathered} \text { EWMA } \\ b=2.1239 \times 10^{-13} \end{gathered}$ | Modified EWMA $b=9.600579 \times 10^{-6}$ | EWMA $b=4.0308 \times 10^{-13}$ | $\begin{gathered} \text { Modified EWMA } \\ b=1.2801949 \times 10^{-5} \end{gathered}$ |
| 0.0007 | 415.503914 | 19.307837* | 351.191004 | 17.937223* | 202.151348 | 17.289440* |
| 0.0009 | 394.328865 | 15.245271* | 320.856371 | 14.171951* | 170.215918 | 13.665109* |
| 0.0010 | 384.125979 | 13.807393* | 307.136133 | 12.840435* | 157.387407 | 12.383952* |
| 0.0030 | 230.568928 | 5.011479* | 146.767998 | 4.707794* | 54.533946 | 4.564598* |
| 0.0050 | 141.203211 | 3.229155* | 81.398115 | 3.062145* | 27.781114 | 2.983359* |
| 0.0070 | 88.045417 | 2.471605* | 48.796600 | 2.362680* | 16.357609 | 2.311262* |
| 0.0090 | 55.861517 | 2.057219* | 30.752391 | 1.979945* | 10.453770 | 1.943442* |
| RMI | 24.968946 | 0 | 18.129071 | 0 | 8.344739 | 0 |

*The smallest $A R L$ on each shift size according to the case.

From the results in Tables 6 and 7, it is evident that the $A R L$ values derived from the explicit formulas for the modified EWMA control chart are less than those for the EWMA control chart for every value of $\lambda$. For example, in Table 6 when $\lambda=0.05$ and shift $=0.009$, the $A R L$ is 197.600498 from the EWMA control chart while the ARL is 11.428518 from the modified EWMA control chart. This corresponds to an RMI value of 0 for the modified EWMA control chart, which is less than that for the EWMA control chart. The results from Tables 6 and 7 are plotted on the charts in Figures. 1 and 2, respectively.


Figure 1. Comparison of the $A R L$ for an $\operatorname{ARX}(1,1)$ on EWMA and modified EWMA control charts for real data in table 6 , where $\lambda=0.10$.


Figure 2. Comparison of the $A R L$ for an $\operatorname{ARX}(2,1)$ on EWMA and modified EWMA control charts for real data in table 7, where $\lambda=0.15$.

From Figures 1 and 2, it can be seen that the $A R L$ values derived from the explicit formulas for the modified EWMA control chart are less than those for the EWMA control chart for every case. For example, in Figure 1, when shift $=0.009$, the $A R L$ from the modified EWMA control chart $(A R L=11.355250)$ is less than that of the EWMA control chart $(A R L=220.280627)$.

From Tables 6 and 7 and Figures 1 and 2, it is evident that the $A R L$ for the modified EWMA control chart is smaller than that of the EWMA control chart for every case. Such that the $A R L$ values derived from the explicit formulas for the modified EWMA control chart outperformed that for the EWMA control chart.

## 8. Conclusions

In this study, we derived explicit formulas for the ARLs on the EWMA and modified EWMA control charts for an $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process with exponential white noise using realworld data observations and compared the performance of the $A R L$ of an $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process on both control charts using the RMI. The suggested formulas are easy to calculate and program. The explicit formulas clearly take much less computational time than the numerical Integral Equation method (NIE). Our results show that they performed better for an $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process on the modified EWMA control chart compared to the EWMA control chart for the case of a onesided shift with constant $k$. However, the conclusions drawn in this study are only applicable to an $\operatorname{ARX}(p, r)$ process and may not be relevant for other processes. In future work, it would be of interest to derive explicit formulas for the $A R L$ of other control charts and processes using the Fredholm integral equation of the second type technique. Based on the findings, the $A R L$ explicit formula for an $\operatorname{ARX}(\mathrm{p}, \mathrm{r})$ process on the modified EWMA control chart outperformed the EWMA control chart. Thus, the modified EWMA control chart could be applied to other processes.

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